

# Constitutive equation of chemo-hyperelasticity

Stress expressions for the solid parts of the mixture.

$$\underline{\underline{\tau}}^{gs} = \frac{\partial \underline{W}^{gs}}{\partial \underline{\underline{E}}_G} \quad , \quad \underline{\underline{\tau}}^c = \frac{\partial \underline{W}^c}{\partial \underline{\underline{E}}_G}$$

In terms of Cauchy stress

$$\underline{\underline{\sigma}}^{gs} = \frac{1}{\det \underline{F}} \cdot \underline{F} \cdot \frac{\partial \underline{W}^{gs}}{\partial \underline{\underline{E}}_G} \cdot \underline{F}^T$$

A quadratic form for  $\underline{W}^{gs}$  in terms of  $\underline{\underline{E}}_G$

$$\underline{W}^{gs} = \frac{1}{2} \lambda (\text{tr } \underline{\underline{E}}_G)^2 + \mu \underline{\underline{E}}_G : \underline{\underline{E}}_G \quad \lambda, \mu: \text{Lame constants}$$

$\underline{\underline{E}}_G$ : may refer to large strains

$$\hookrightarrow = \frac{1}{8} (\lambda + 2\mu) \underline{I}_1^2(\underline{\underline{C}}) - \frac{1}{4} (3\lambda + 2\mu) \underline{I}_1(\underline{\underline{C}}) - \frac{1}{2} \mu \underline{I}_2(\underline{\underline{C}}) + \frac{3}{8} (3\lambda + 2\mu)$$

$\underline{I}_1, \underline{I}_2$ : 1<sup>st</sup> and 2<sup>nd</sup> scalar invariants of the right Cauchy-Green deformation tensor  $\underline{\underline{C}}$ .

$$\underline{I}_1 = \underline{I}_1(\underline{\underline{C}}) = \text{tr } \underline{\underline{C}}$$

$$\underline{I}_2 = \underline{I}_2(\underline{\underline{C}}) = \frac{1}{2} [\underline{I}_1^2(\underline{\underline{C}}) - \underline{\underline{C}} : \underline{\underline{C}}]$$

$$\underline{\underline{\tau}}^{gs} = \frac{\partial \underline{W}^{gs}}{\partial \underline{\underline{E}}_G} \quad \underline{\underline{C}} = 2 \underline{\underline{E}}_G + \underline{I} \quad \text{gives a linear stress-strain relation}$$

If we use

$$\underline{W}^{gs} = \underline{W}_0^{gs} f$$

where  $\underline{W}_0^{gs}$  is the quadratic form above and  $f = f(\underline{\underline{C}})$  a non linear <sup>scalar</sup> function of  $\underline{\underline{C}}$ , we can make the  $\underline{W}^{gs}$  strongly non linear, in order to get a non-linear stress-strain relation.



Mass balance of ions in the EF phase

$$\frac{1}{\det F} \frac{dN_{kE}}{dt} + \operatorname{div} \vec{J}_{kE} = 0$$

Electrochemical potentials of the  $k$ th ion:  $\mu_{kE}^{ec}$

$k$ : refers to the  $k$ th ion

$N_{kE}$ : molar mass measure of the  $k$ th ion in the Extracellular phase

Vector of unknown quantities

$$\vec{X} = \begin{bmatrix} \vec{u} \\ g_{WE}^{ec} \\ g_{NaE}^{ec} \\ g_{ClE}^{ec} \end{bmatrix} \quad 3 + N_{sd} \text{ unknowns}$$

Purely mechanical contribution with non-linear aspects

For a collagen fibril, the mapping from the undeformed to the deformed configuration, regarding its direction, is given by the relation

$$\vec{m} = \frac{\vec{F} \cdot \vec{m}}{|\vec{F} \cdot \vec{m}|}$$

$\vec{m}$ : directional unit vector of the collagen fibril in the deformed configuration

$\vec{m}$ : ... in undeformed configuration

Accordingly, the 2<sup>nd</sup> order structure tensors  $\underline{\underline{M}}$  and  $\underline{\underline{M}}$  are related by the relation

$$\underline{\underline{M}} = \vec{m} \otimes \vec{m} = \frac{\vec{F} \cdot \underline{\underline{M}} \cdot \vec{F}^T}{|\vec{F} \cdot \vec{m}|^2}$$

For an one family of parallel fibers we have transverse isotropy (perpendicular to the single direction of the fibers)

The strain energy density function for a transversely isotropic material, is written in terms of the following strain invariants

$$I_1 = \text{tr} \underline{\underline{C}} \quad \underline{\underline{C}}: \text{Right Cauchy-Green deformation tensor}$$

$$I_2 = \frac{1}{2} [\text{tr}^2 \underline{\underline{C}} - \text{tr} \underline{\underline{C}}^2]$$

$$I_3 = \det \underline{\underline{C}}$$

~~When~~ Writing a  $\underline{W}$  in terms of  $I_1, I_2, I_3$  i.e.  $\underline{W} = \underline{W}(I_1, I_2, I_3)$  we refer to an isotropic material. For a transversely isotropic material, we use the following extra "invariants" (pseudo-invariants)

$$I_4 = \underline{\underline{C}} : \underline{\underline{M}}$$

$$I_5 = \underline{\underline{C}}^2 : \underline{\underline{M}}$$

A  $\underline{W} = \underline{W}(I_1, I_2, I_3, I_4, I_5)$  is associated with a transversely anisotropic material, with preferred anisotropy direction the  $\underline{\underline{m}}$  (one indicated by  $\underline{\underline{m}}$  where

$\underline{\underline{M}} = \underline{\underline{m}} \otimes \underline{\underline{m}}$ ). The presence of  $I_3$  in the form of  $\underline{W}$  indicates a compressible material, like  $\underline{W} = \underline{W}(I_1, I_2, I_3)$ . A form like  $\underline{W} = \underline{W}(I_1, I_2)$  indicates an isotropic incompressible material. Similarly a form like  $\underline{W} = \underline{W}(I_1, I_2, I_4, I_5)$  indicates a transversely isotropic material, which is incompressible.

$I_3 \rightarrow$  relates to the volume change

$I_4 \rightarrow$  is related to the extension of the fibers along their direction

$I_5 \rightarrow$  no direct physical meaning, but is related to shear along directions perpendicular to the fiber direction.

For an incompressible <sup>and inextensible</sup> transversely isotropic material

$$\underline{W} = \underline{w}(I_1, I_2) + \frac{1}{2} P_F (I_3 - 1) + \frac{1}{2} T (I_4 - 1)$$

The stresses for this material are given by the formula:

$$\underline{\underline{\tau}} = 2 \frac{\partial \underline{W}}{\partial \underline{\underline{C}}} \Rightarrow \underline{\underline{\tau}} = 2 \frac{\partial \underline{W}}{\partial \underline{\underline{C}}} - \underbrace{P_F \det \underline{\underline{C}}^{-1}}_{\text{Incompressibility term}} + \underbrace{T M}_{\text{Inextensibility term}}$$

The extra parameters  $P_F$ , and  $T$  are found ~~for~~ from equilibrium equation or from boundary condition.