

Constitutive equation of chemo-hyperelasticity

Stress expressions for the solid parts of the mixture.

$$\underline{\underline{\sigma}}^{\text{ss}} = \frac{\partial \underline{\underline{W}}^{\text{ss}}}{\partial \underline{\underline{E}}_G}, \quad \underline{\underline{\epsilon}}^c = \frac{\partial \underline{\underline{W}}^c}{\partial \underline{\underline{E}}_G}$$

In terms of Cauchy stress

$$\underline{\underline{\sigma}}^{\text{ss}} = \frac{1}{\det \underline{\underline{F}}} \cdot \underline{\underline{F}} \cdot \frac{\partial \underline{\underline{W}}^{\text{ss}}}{\partial \underline{\underline{E}}_G} \cdot \underline{\underline{F}}^T$$

A quadratic form for $\underline{\underline{W}}^{\text{ss}}$ in terms of $\underline{\underline{E}}_G$

$$\underline{\underline{W}}^{\text{ss}} = \frac{1}{2} \lambda (\text{tr} \underline{\underline{E}}_G)^2 + \mu \underline{\underline{E}}_G : \underline{\underline{E}}_G = \quad \lambda, \mu: \text{Lame constants}$$

$\underline{\underline{E}}_G$: may refer to large strains

$$\begin{aligned} \underline{\underline{W}}^{\text{ss}} &= \frac{1}{8} (\lambda + 2\mu) I_1^2(\underline{\underline{C}}) + \frac{1}{4} (3\lambda + 2\mu) I_1(\underline{\underline{C}}) - \frac{1}{2} \mu I_2(\underline{\underline{C}}) \\ &\quad + \frac{3}{8} (3\lambda + 2\mu). \end{aligned}$$

I_1, I_2 : 1st and 2nd scalar invariants of the right Cauchy-Green deformation tensor $\underline{\underline{C}}$.

$$I_1 = I_1(\underline{\underline{C}}) = \text{tr} \underline{\underline{C}}$$

$$I_2 = I_2(\underline{\underline{C}}) = \frac{1}{2} [I_1^2(\underline{\underline{C}}) - \underline{\underline{C}} : \underline{\underline{C}}]$$

$$\underline{\underline{C}} = 2 \underline{\underline{E}}_G + \underline{\underline{I}}$$

$\underline{\underline{\sigma}}^{\text{ss}} = \frac{\partial \underline{\underline{W}}^{\text{ss}}}{\partial \underline{\underline{E}}_G}$ gives a linear stress-strain relation

If we use

$$\underline{\underline{W}}^{\text{ss}} = \underline{\underline{W}}_0^{\text{ss}} f$$

where $\underline{\underline{W}}_0^{\text{ss}}$ is the quadratic form above and $f = f(\underline{\underline{C}})$ a non-linear function of $\underline{\underline{C}}$, we can make the $\underline{\underline{W}}^{\text{ss}}$ strongly nonlinear, in order to get a non-linear stress-strain relation.

$$\text{If } f = f(\zeta) = \exp[\alpha(\det(\zeta) - 1)]$$

the stress-strain relation becomes nonlinear.
If $f = f(\zeta) = 1$ we get linear stress-strain relation.

For the collagen fibrils, we may have (for a single fibril)

$$w_c = w_c(L^2)$$

$$L = \frac{1}{2} \langle \zeta : \underline{\underline{M}}_c - 1 \rangle = \langle \underline{\underline{E}}_G : \underline{\underline{M}}_c \rangle$$

$\langle \rangle$: denote the positive part of the quantity inside

$\underline{\underline{M}}_c$: 2nd order structure tensor related to the undeformed direction of the single collagen fibril

$$\underline{\underline{M}}_c = \underline{\underline{m}}_c \otimes \underline{\underline{m}}_c$$

$\underline{\underline{m}}_c$: unit vector indicating the direction of a single collagen fiber in the undeformed configuration.

$\langle \underline{\underline{E}}_G : \underline{\underline{M}}_c \rangle$: a deformation (scalar) measure of the stretch of the fiber along its direction.

For example we can write

$$w_c = \frac{k_c}{2k_c} (\exp(k_c L^2) - 1)$$

where k_c , k_c appropriate stiffness constants

For a network of two fibers, we write

$$W_c(E_G) = \sum_{i=1}^2 \frac{k_i}{2k_i} [\exp(k_i L_i^2) - 1]$$

where

$$L_i = \langle \underline{\underline{E}}_G : \underline{\underline{M}}_{ci} \rangle$$

Governing equations for the cornea
Nature

Field eq.

Unknowns

Momentum balance

$$\operatorname{div} \vec{\underline{\underline{\sigma}}} = \vec{0}$$

Displacement \vec{u}

Mass balance

$$\operatorname{div} \vec{v}_s + \operatorname{div} \vec{J}_E$$

Chemical potential of EF water SWE

Mass balance
of ions in the
EF phase

$$\frac{1}{\det F} \frac{dN_{KE}}{dt} + \operatorname{div} \vec{J}_{KE} = 0$$

Electroche-
mical poten-
tials of the
kth ion: φ_{KE}^{ec}

k: refers to the kth ion

N_{KE} : molar mass measure of
the kth ion in the
Extrafibrillar phase

Vector of unknown quantities

$$\vec{x} = \begin{bmatrix} \vec{u} \\ \varphi_{WE}^{ec} \\ \varphi_{NaE}^{ec} \\ \varphi_{ClE}^{ec} \end{bmatrix}$$

3 + Nsd unknowns

Purely mechanical contribution with
non-linear aspects

For a collagen fibril, the mapping
from the undeformed to the deformed
configuration, regarding its direction,
is given by the relation

$$\vec{m} = \frac{\vec{F} \cdot \vec{m}_0}{|\vec{F} \cdot \vec{m}|}$$

\vec{m} : directional unit
vector of the collagen
fibril in the deformed
configuration

\vec{m}_0 : ... in undeformed configuration

Accordingly, the 2nd order structure
tensors $\underline{\underline{M}}$ and $\underline{\underline{M}}_0$ are related by the
relation

$$\underline{\underline{M}} = \vec{m} \otimes \vec{m} = \frac{\vec{F} \cdot \underline{\underline{M}}_0 \cdot \vec{F}^T}{|\vec{F} \cdot \vec{m}|^2}$$

For an one family of parallel fibers
we have transverse isotropy (perpen-
dicular to the single direction of the fibers)

The strain energy density function for a transversely isotropic material, is written in terms of the following strain invariants

$$I_1 = \text{tr}(\underline{\underline{\zeta}})$$

ζ : Right Cauchy-Green deformation tensor

$$I_2 = \frac{1}{2} [\text{tr}^2 \underline{\underline{\zeta}} - \text{tr}(\underline{\underline{\zeta}}^2)]$$

$$I_3 = \det \underline{\underline{\zeta}}$$

~~With~~ Writing a $\underline{\underline{W}}$ in terms of I_1, I_2, I_3 i.e $\underline{\underline{W}} = \underline{\underline{W}}(I_1, I_2, I_3)$ we refer to an isotropic material. For a transversely isotropic material, we use the following extra "invariants" (pseudo-invariants)

$$I_4 = \underline{\underline{\zeta}} : \underline{\underline{M}}$$

$$I_5 = \underline{\underline{\zeta}}^2 : \underline{\underline{M}}$$

$$\text{A } \underline{\underline{W}} = \underline{\underline{W}}(I_1, I_2, I_3, I_4, I_5)$$

is associated with a transversely anisotropic material, with preferred anisotropy direction the \vec{m} (one indicated by \vec{m} where

$\underline{\underline{M}} = \vec{m} \otimes \vec{m}$). The presence of I_3 in the form of $\underline{\underline{W}}$ indicates a compressible material, like $\underline{\underline{W}} = \underline{\underline{W}}(I_1, I_2, I_3)$.

A form like $\underline{\underline{W}} = \underline{\underline{W}}(I_1, I_2)$ indicates an isotropic incompressible material.

Similarly a form like $\underline{\underline{W}} = \underline{\underline{W}}(I_1, I_2, I_4, I_5)$ indicates a transversely isotropic material, which is incompressible.

$I_3 \rightarrow$ relates to the volume change

$I_4 \rightarrow$ is related to the extension of the fibers along their direction

$I_5 \rightarrow$ no direct physical meaning, but is related to shear along directions perpendicular to the fiber direction.
and inextensible

For an incompressible transversely isotropic material

$$\underline{W} = \underline{w}(I_1, I_2) + \frac{1}{2} P_F (I_3 - 1) + \frac{1}{2} T (I_4 - 1)$$

The stresses for this material are given by the formula:

$$\underline{\underline{\sigma}} = 2 \frac{\partial \underline{W}}{\partial \underline{\underline{C}}} \Rightarrow \underline{\underline{\sigma}} = 2 \frac{\partial \underline{W}}{\partial \underline{\underline{C}}} - \underbrace{P_F \det \underline{\underline{C}} \underline{\underline{C}}^{-1}}_{\text{Incompressibility term}} + \underbrace{T \underline{\underline{M}}}_{\text{Inextensibility term}}$$

The extra parameters P_F and T are found from equilibrium equation or from boundary condition.