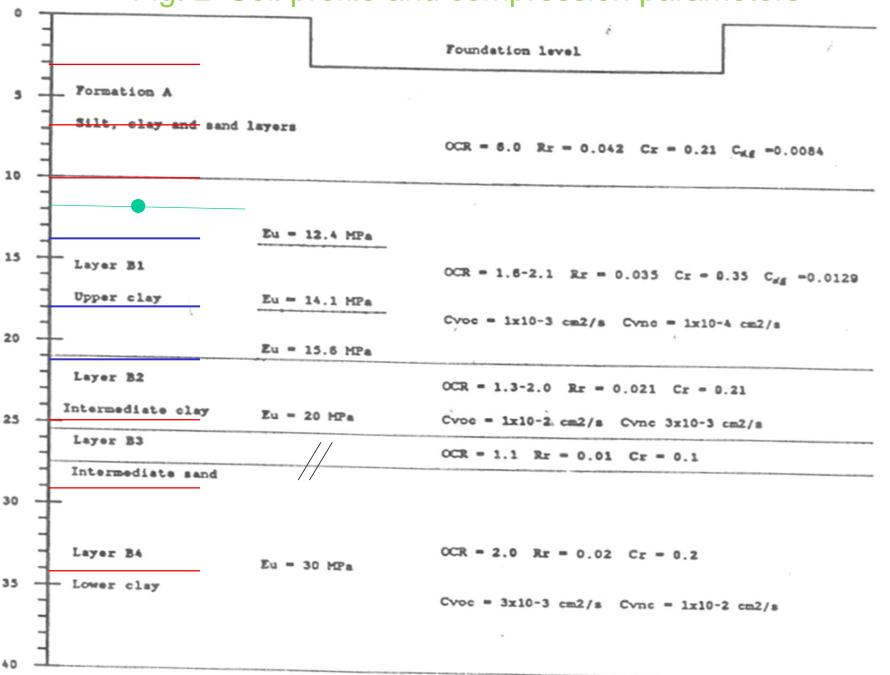
MSC IN ANALYSIS AND DESIGN OF EARTHQUAKE RESISTANT STRUCTURES (ADERS)

Course: Geotechnical Engineering in the Design of Structures

PROJECT: SETTLEMENT CALCULATIONS FOR THE LEANING TOWER OF PISA

- The leaning Tower of Pisa was designed as a circular bell tower of 19.06m in diameter. The tilt of the Tower (before the period of strengthening 1990-2001) is shown in Fig. 1.
- The first stage of construction took place in the period 1173-1178 and the load applied by three floors to the foundation was 92904kN. Settlement was introduced during this stage.
- The second stage of construction took place in the period 1272-1278 and the total load applied to the foundation was 134534kN.
- The third stage of construction in the period 1360-1370 resulted in total load of 141640kN.
- Calculate the settlement of the Tower until 1990 when a multinational task force of engineers started work on its stabilization. The soil profile and the parameters required for settlement calculations are given in Figs 2,3 and 4.

Fig. 2 Soil profile and compression parameters



$$E_u = \frac{\Delta \sigma}{\varepsilon_z}$$

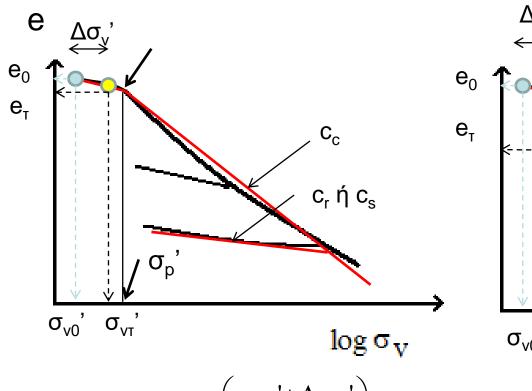
Immediate settlement, ρ_i

$$\rho = H \frac{c_r}{1 + e_0} \log \left(\frac{\sigma_{v0}' + \Delta \sigma_{v}'}{\sigma_{v0}'} \right)$$
 Consolidation settlement, ρ_c

 $\delta_s = h_s C_{\alpha \epsilon} \log_{10}(t/t_s)$ where $t_s = time$ of completion of primary consolidation, h_s =depth of layer at the beginning of secondary consolidation

Secondary settlement, ρ_s

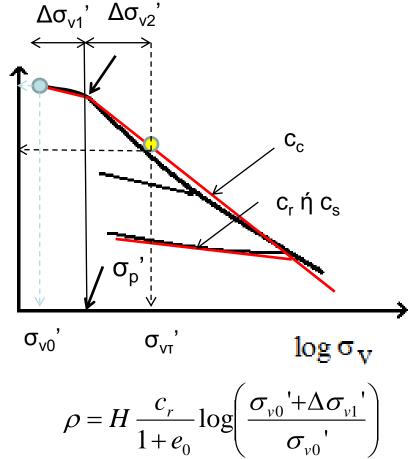
Consolidation settlement pc



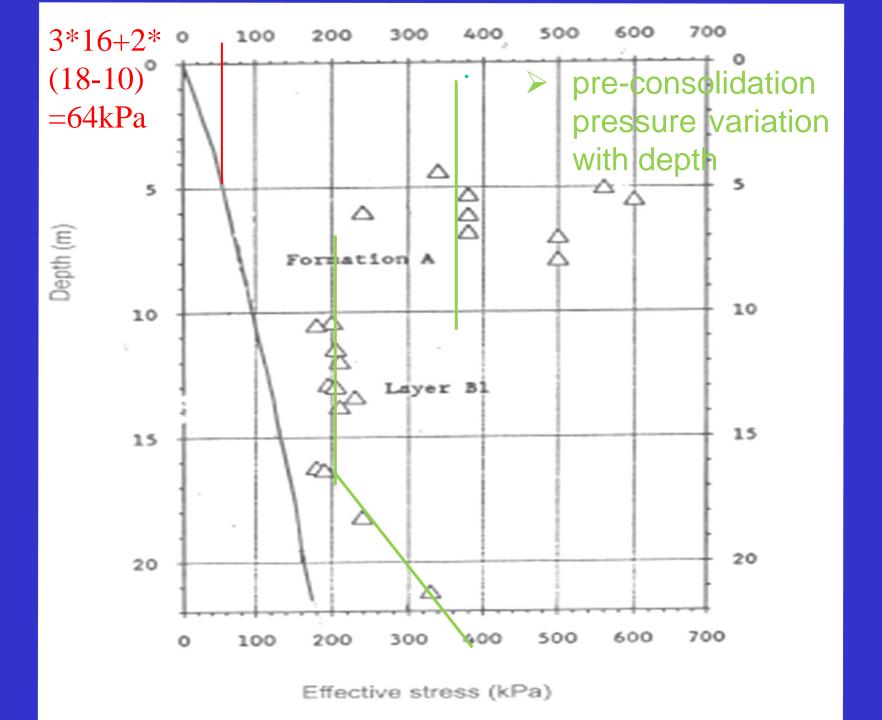
$$\rho = H \frac{c_r}{1 + e_0} \log \left(\frac{\sigma_{v0}' + \Delta \sigma_{v}'}{\sigma_{v0}'} \right)$$

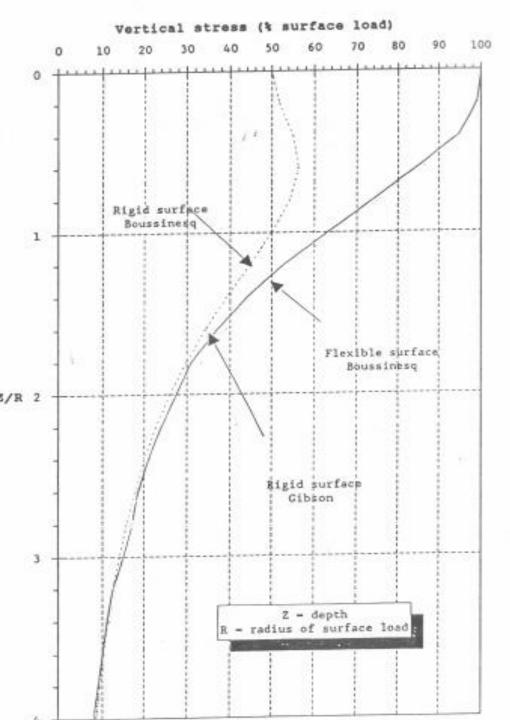
 σ_p ' = pre-consolidation stress

$$\sigma_{v0}$$
' σ_{p} '
$$OCR = \frac{\sigma_{p}}{\sigma_{v0}}$$



$$+H\frac{c_c}{1+e_0}\log\left(\frac{\sigma_p'+\Delta\sigma_{v2}'}{\sigma_p'}\right)$$

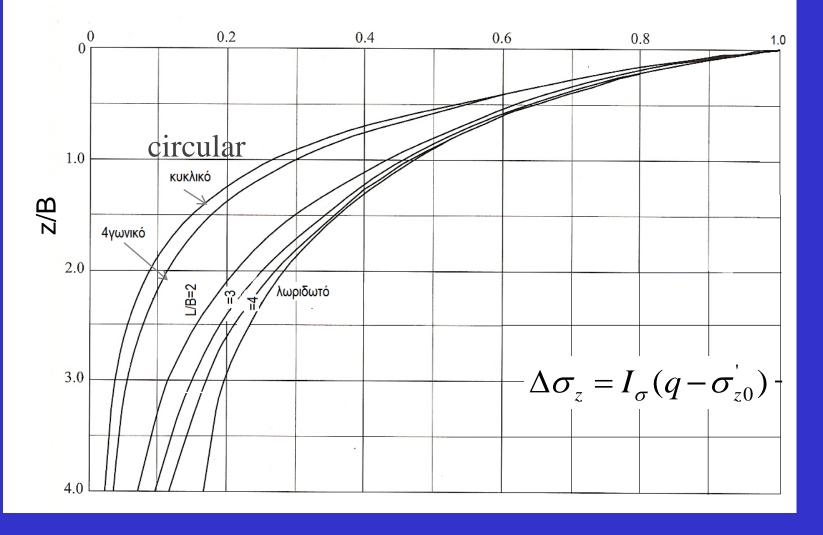




Vertical stress distribution with depth under circular foundation

$$\Delta \sigma_z = \left[1 - \left(\frac{1}{1 + \left(\frac{B}{2z}\right)^2}\right)^a\right] (q - \sigma_{z0}')$$

Poulos & Davis 1974 used Boussinesq's equations to calculate stresses on the centre line under a circular footing (α =2.6, B=width of footing)



Stresses under the centre line of rigid footing (Butterfield & Banerjee 1971)



 σ_{z0} '=normal effective stress at depth D